

## CLAIMS

1. A device (10) for generating a noise signal, comprising a noise source (11) for generating intrinsic  
5 noise, **characterized** in that the noise source (11) is a noisy amplifier cell (100) having an amplifying means (103a, 103b), a load (101a, 101b, 102a, 102b) connected to said amplifying means and supply, and a tail-current source (104a, 104b) connected to grounding means and to the  
10 amplifying means (103a, 103b).

2. The device according to claim 1, wherein the amplifying means comprises a common-source amplifier (103a, 103b).  
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3. The device according to claim 2, wherein the common source amplifier (103a, 103b) comprises transistors (103a, 103b) having a differential topology.

20 4. The device according to any of the claims 1-3, wherein the load comprises cascoded transistors (101a, 101b, 102a, 102b).

25 5. The device according to any of the claims 1-4, wherein the load comprises resistors.

6. The device according to any of the claims 2-5, wherein the tail-current source (104a, 104b) is connected to the amplifying means (103a, 103b) and grounding means to  
30 provide common-mode feedback.

7. The device according to any of the claims 1-6, further comprising a first amplifier cell (200) being DC coupled to the noisy amplifier cell (100), the output  
35 terminals (105a, 105b) of the noisy amplifier cell (100)

are connected to respective input terminals (206a, 206b) of the first amplifier (200).

8. The device according to claim 7, wherein the  
5 design of the first amplifier (200) corresponds to the design of the noisy amplifier cell (100).

9. The device according to claim 7 or 8, further  
comprising a differential amplifier (300) having first and  
10 second input terminals (306a, 306b) connected to output terminals (205a, 205b) of the first amplifier (200), said differential amplifier comprising an amplifying means (303a, 303b), a load (301a, 301b, 302a, 302b) connected to said amplifying means and supply, and a tail-current source  
15 (304a, 304b) connected to grounding means and to said amplifying means.

10. The device according to any of the claims 1-9, wherein the load (101a, 101b, 102a, 102b; 201a, 201b, 202a, 202b; 301a, 301b, 302a, 302b), the amplifying means (103a, 103b; 203a, 203b; 303a, 303b), and the tail-current source (104a, 104b; 204a, 204b; 304a, 304b) of the noisy amplifier cell (100), the first amplifier (200) and a differential  
20 amplifier (300), comprises MOS (Metal Oxide Semiconductor) transistors.  
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11. The device according to any of the claims 1-9, wherein the load, the amplifying means, and the tail-current source of the noisy amplifier cell (100), the first  
30 amplifier (200) and a differential amplifier (300), comprises BJT (Bipolar Junction Transistors) transistors.

12. The device according to any of the claims 1-9, wherein the load comprises PMOS transistors (101a, 101b,  
35 102a, 102b; 201a, 201b, 202a, 202b; 301a, 301b, 302a,

302b), and the amplifying means and the tail-current source comprise NMOS transistors (103a, 103b, 104a, 104b; 203a, 203b, 204a, 204b; 303a, 303b, 304a, 304b).

5           13. The device according to claim any of the claims 1-9, wherein the load comprises NMOS transistors, and the amplifying means and the tail-current source comprises PMOS transistors.

10           14. The device according to claim 12 or 13, wherein the width-over-length ratio (Z) of the transistors (103a, 103b) of the amplifying means is at least 3 times the width-over-length ratio of the transistors (104a, 104b) of the tail-current source, and the width-over-length ratio of  
15 the second transistor pair (102a, 102b) of the load is at least 3 times the size of the width-over-length ratio of the first transistor pair (101a, 101b) of the load.

20           15. The device according to claim 12 or 13, wherein the width (W) of the transistors (103a, 103b) of the amplifying means and the transistors of the second transistor pair (102a, 102b) of the load is in the range of 2,5-125  $\mu\text{m}$ , and the length (L) of said transistors is in the range of 0,25-12,5  $\mu\text{m}$ ; the width and the length of the  
25 transistors (104a, 104b) of the tail-current source and the transistors of the first transistor pair (101a, 101b) of the load are in the range of 0,25-12,5  $\mu\text{m}$ .

30           16. The device according to any of the claims 1-15, wherein input terminals (106a, 106b) of the amplifying means (103a, 103b) of the noisy amplifier cell (100) are short-circuited AC-wise to grounding means.

35           17. The device according to any of the claims 1-15, wherein input terminals (106a, 106b) of the amplifying

means (103a, 103b) of the amplifier cell (100) are short-circuited DC-wise to a fixed potential.

18. The device according to claim 7, further  
5 comprising a DC compensation loop having a feedback filter (15) connected to the output terminals (205a, 205b) of the first amplifier (200) and to the input terminals (106b, 106a) of the noisy amplifier (100), respectively.

10 19. The device according to claim 18, wherein the feedback filter (15) comprises first and second filters (700a, 700b) each comprising a high-frequency phantom zero capacitor ( $C_z$ , 705) providing phase compensation.

15 20. The device according to claim 18 or 19, wherein the feedback filter (15) comprises two filters (700a, 700b) each comprising a first capacitor ( $C_p$ , 707a-707e) connected to grounding means and a first resistor ( $R_1$ , 703) being connected to the output terminal of the filter (700a,  
20 700b), a second resistor ( $R_2$ , 702a-702b) in parallel to the high-frequency phantom zero capacitor ( $C_z$ , 705) connected to the output terminal of the filter (700a, 700b) and to a third resistor ( $R_3$ , 701a-701b) being connected to the input terminal of the filter (700a, 700b).

25 21. The device according to claim 20, wherein the first capacitor ( $C_p$ , 707a-707e), the first resistor ( $R_1$ , 703), the second resistor ( $R_2$ , 702a-702b), the high-frequency phantom zero capacitor ( $C_z$ , 705), and the third  
30 resistor ( $R_3$ , 701a-701b) comprises MOS transistors.

22. The device according to claim 20, wherein the first capacitor ( $C_p$ , 707a-707e) comprises NMOS transistors, and the first resistor ( $R_1$ , 703), the second resistor ( $R_2$ ,

702a-702b), and the third resistor ( $R_3$ , 701a-701b) comprises PMOS transistors.

23. The device according to claim 20, wherein the  
5 first capacitor ( $C_p$ , 707a-707e) comprises PMOS transistors, and the first resistor ( $R_1$ , 703), the second resistor ( $R_2$ , 702a-702b), and the third resistor ( $R_3$ , 701a-701b) comprises NMOS transistors.

10 24. The device according to any of the previous claims, wherein an output terminal (305) of said device (10) is connected to a device for generating a random sequence of bits (10), comprising an oscillating means having an input terminal (409) for receiving a bias as  
15 input connected to said output terminal (305), the oscillating means (13) comprises at least one oscillator amplifier (400a, 400b, 400c) and a differential amplifier (500) connected to said oscillator amplifier, each oscillator amplifier (400a, 400b, 400c) and the  
20 differential amplifier (500) comprise an amplifying means (303a, 303b; 403a, 403b) protected from interfering signals by means of a load (301a, 301b, 302a, 302b; 401a, 401b, 402a, 402b) connected to said amplifying means and supply, and a tail current source (304a, 304b; 404a, 404b)  
25 connected to said amplifying means and grounding means.

25. An electronic apparatus (1) comprising a device (10) for generating a noise signal according to any of the claims 1-24.

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26. The electronic apparatus according to claim 25, wherein the apparatus is a mobile radio terminal, a pager, a communicator, an electronic organizer or a smartphone.

27. The electronic apparatus according to claim 25,  
wherein the apparatus is a mobile telephone (1).

28. An integrated circuit comprising a device (10)  
5 for generating a noise signal according to any of the  
claims 1-24.